

Kinematics for Lynxmotion Robot Arm

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Note: This article contains text and two graphics from the reference [1] listed at the end.

Kinematics

Forward Kinematics

Given the joint angles and the links geometry, compute the orientation of the end effector relative to the base frame.

Inverse Kinematics

Given the position and orientation of the end effector relative to the base frame compute all possible sets of joint angles and link geometries which could be used to attain the given position and orientation of the end effector.

2R Planar Manipulator

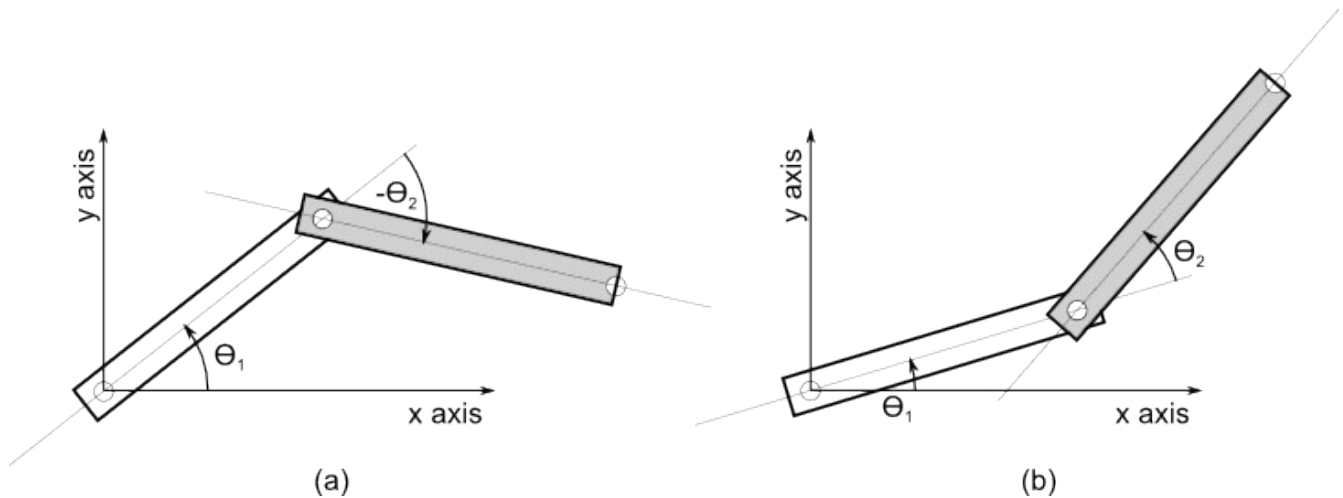


Figure 1: Elbow up (a) and Elbow down (b) configuration of a 2R planar manipulator

Forward Kinematics

$$x = l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2)$$

$$y = l_1 \sin \theta_1 + l_2 \cdot \sin(\theta_1 + \theta_2)$$

Inverse Kinematics

$$\begin{aligned}x^2 + y^2 &= l_1^2 \cos^2 \theta_1 + l_2^2 \cos^2 (\theta_1 + \theta_2) + 2l_1 l_2 \cos \theta_1 \cos (\theta_1 + \theta_2) + \\&\quad l_1^2 \sin^2 \theta_1 + l_2^2 \sin^2 (\theta_1 + \theta_2) + 2l_1 l_2 \sin \theta_1 \sin (\theta_1 + \theta_2) \\&= l_1^2 + l_2^2 + 2l_1 l_2 [\cos \theta_1 \cos (\theta_1 + \theta_2) + \sin \theta_1 \sin (\theta_1 + \theta_2)]\end{aligned}$$

Next we use the following equalities:

$$\begin{aligned}\sin (x \pm y) &= \sin x \cos y \pm \cos x \sin y \\ \cos (x \pm y) &= \cos x \cos y \mp \sin x \sin y\end{aligned}$$

Therefore

$$\begin{aligned}x^2 + y^2 &= l_1^2 + l_2^2 + 2l_1 l_2 [\cos \theta_1 (\cos \theta_1 \cos \theta_2 - \sin \theta_1 \sin \theta_2) + \sin \theta_1 (\sin \theta_1 \cos \theta_2 + \cos \theta_1 \sin \theta_2)] \\&= l_1^2 + l_2^2 + 2l_1 l_2 [\cos^2 \theta_1 \cos \theta_2 + \sin^2 \theta_2 \cos \theta_2] \\&= l_1^2 + l_2^2 + 2l_1 l_2 \cos \theta_2\end{aligned}$$

and

$$\cos \theta_2 = \frac{x^2 + y^2 - l_1^2 - l_2^2}{2l_1 l_2}$$

From here we could get the angle directly using the arccosine function but this function is very inaccurate for small angles. The typical way to avoid this inaccuracy is to convert further until we can use the atan2 function.

$$\cos^2 \theta_2 + \sin^2 \theta_2 = 1$$

$$\sin \theta_2 = \pm \sqrt{1 - \cos^2 \theta_2}$$

The two solutions correspond to the 'elbow up' and 'elbow down' configurations as shown in figure 1 a) and b).

Finally we get:

$$\begin{aligned}\theta_2 &= \text{atan2}(\sin \theta_2, \cos \theta_2) = \\&= \text{atan2}(\pm \sqrt{1 - \cos^2 \theta_2}, \cos \theta_2) = \\&= \text{atan2}\left(\pm \sqrt{1 - \left(\frac{x^2 + y^2 - l_1^2 - l_2^2}{2l_1 l_2}\right)^2}, \frac{x^2 + y^2 - l_1^2 - l_2^2}{2l_1 l_2}\right)\end{aligned}$$

For solving θ_1 we rewrite the original nonlinear equations using a change of variables as follows (see figure 2):

$$x = l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2)$$

$$y = l_1 \sin \theta_1 + l_2 \sin(\theta_1 + \theta_2)$$

$$x = k_1 \cos \theta_1 - k_2 \sin \theta_1$$

$$y = k_1 \sin \theta_1 + k_2 \cos \theta_1$$

where

$$k_1 = l_1 + l_2 \cos \theta_2$$

$$k_2 = l_2 \sin \theta_2$$

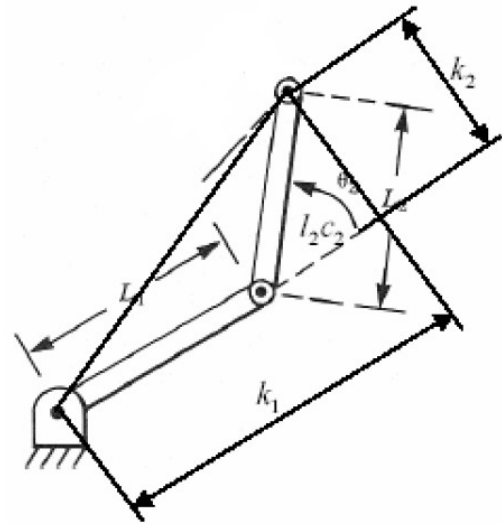


Figure 2 (taken from [1])

Next we change the way we write the constants k_1, k_2 (see figure 3)

$$r = \sqrt{k_1^2 + k_2^2}$$

$$\gamma = \text{atan2}(k_2, k_1)$$

$$k_1 = r \cos \gamma$$

$$k_2 = r \sin \gamma$$

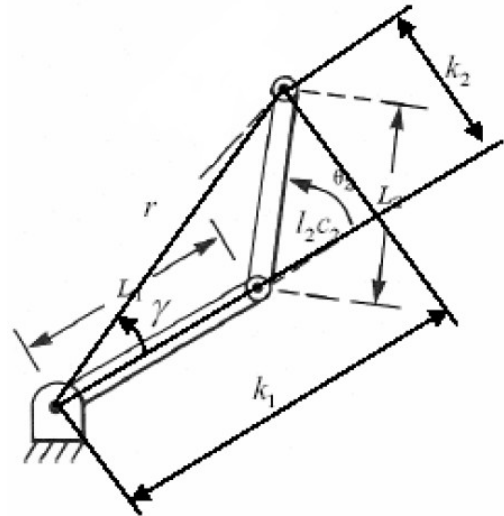


Figure 3 (taken from [1])

Inserting into the previous transformations of x and y yields:

$$x = r \cos \gamma \cos \theta_1 - r \sin \gamma \sin \theta_1$$

$$y = r \cos \gamma \sin \theta_1 + r \sin \gamma \cos \theta_1$$

or

$$\frac{x}{r} = \cos \gamma \cos \theta_1 - \sin \gamma \sin \theta_1$$

$$\frac{y}{r} = \cos \gamma \sin \theta_1 + \sin \gamma \cos \theta_1$$

or

$$\frac{x}{r} = \cos(\gamma + \theta_1)$$

$$\frac{y}{r} = \sin(\gamma + \theta_1)$$

Applying the atan2 function:

$$\gamma + \theta_1 = \text{atan2}\left(\frac{y}{r}, \frac{x}{r}\right) = \text{atan2}(y, x)$$

$$\theta_1 = \text{atan2}(y, x) - \text{atan2}(k_2, k_1)$$

where

$$k_1 = l_1 + l_2 \cos \theta_2$$

$$k_2 = l_2 \sin \theta_2$$

Notes

- Switching to another choice of sign in the solution for θ_2 above will change the sign of k_2 and thus will affect θ_1 .
- If $x = y = 0$ then the solution becomes undefined. In this case θ_1 is arbitrary. Note that this is only possible if both links have the same length and can fold back onto each other.

Inverse Kinematics for Lynxmotion Robot Arm

Here we focus on the inverse kinematics for the wrist without taking the gripper into account. This means the robot arm can be described as a 2R planar manipulator on a rotating base.

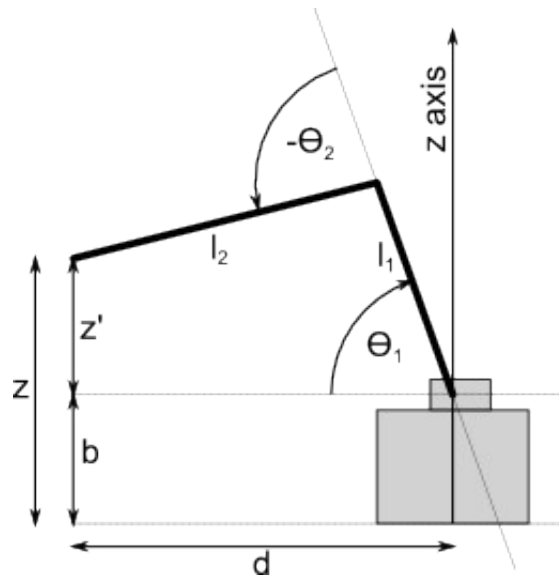


Figure 4: Side view of Lynxmotion robot arm without gripper.

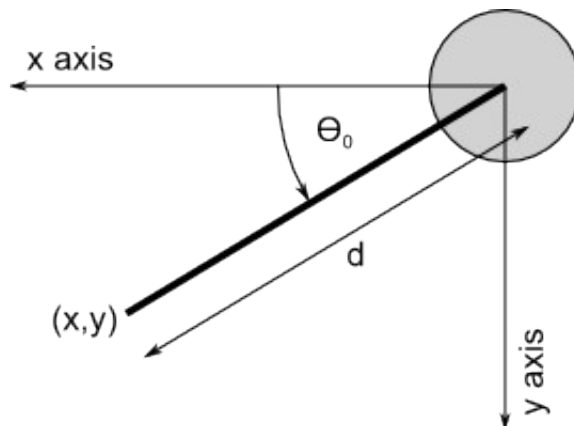


Figure 5: Top view of Lynxmotion robot arm without gripper.

The goal is to calculate the angles $\theta_0, \theta_1, \theta_2$ from the position (x, y, z) of the wrist. Note that the x, y, z axes as illustrated in figures 4 and 5 do not match the default coordinate system used by the RIOS software.

The angle θ_0 is fully defined by the coordinates x and y :

$$\theta_0 = \text{atan2}(y, x)$$

In order to get the other two angles we leverage the distance d of the point (x, y) from the origin and the

height z' above the shoulder joint.

$$d = \sqrt{x^2 + y^2}$$

$$z' = z - b$$

where b is the height of the shoulder joint (see figure 4 for details).

This allows us to use the calculations for the 2R planar manipulator. d is plugged in as the x value into the formulas for θ_1 and θ_2 and z' is used in as the y value.

References

- [1] MECH 498: Introduction to Robotics, Inverse Manipulator Kinematics by M. O'Malley
<http://www.owlnet.rice.edu/~mech498/498lecture4.pdf>
- [2] Stanford University Course: Artificial Intelligence | Introduction to Robotics by Khatib, Oussama
(<http://see.stanford.edu/see/courseInfo.aspx?coll=86cc8662-f6e4-43c3-a1be-b30d1d179743>)
- [3] Theory of Applied Robotics: Kinematics, Dynamics, and Control by Resa N. Jazar
(http://www.amazon.com/Theory-Applied-Robotics-Kinematics-Dynamics/dp/0387324755/ref=sr_1_1?ie=UTF8&s=books&qid=1255828006&sr=8-1)

